



National Alliance  
for Water Innovation

# Enabling High Recovery with Flow Reversal and Feed Flushing

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Thursday, September 19, 2024

# Chino Desalter I

The **Chino Desalter I** is part of the **Chino Desalter Project**, which was established to provide a reliable water supply and manage groundwater quality in the **Chino Basin**, located in Southern California.

## Current Infrastructure

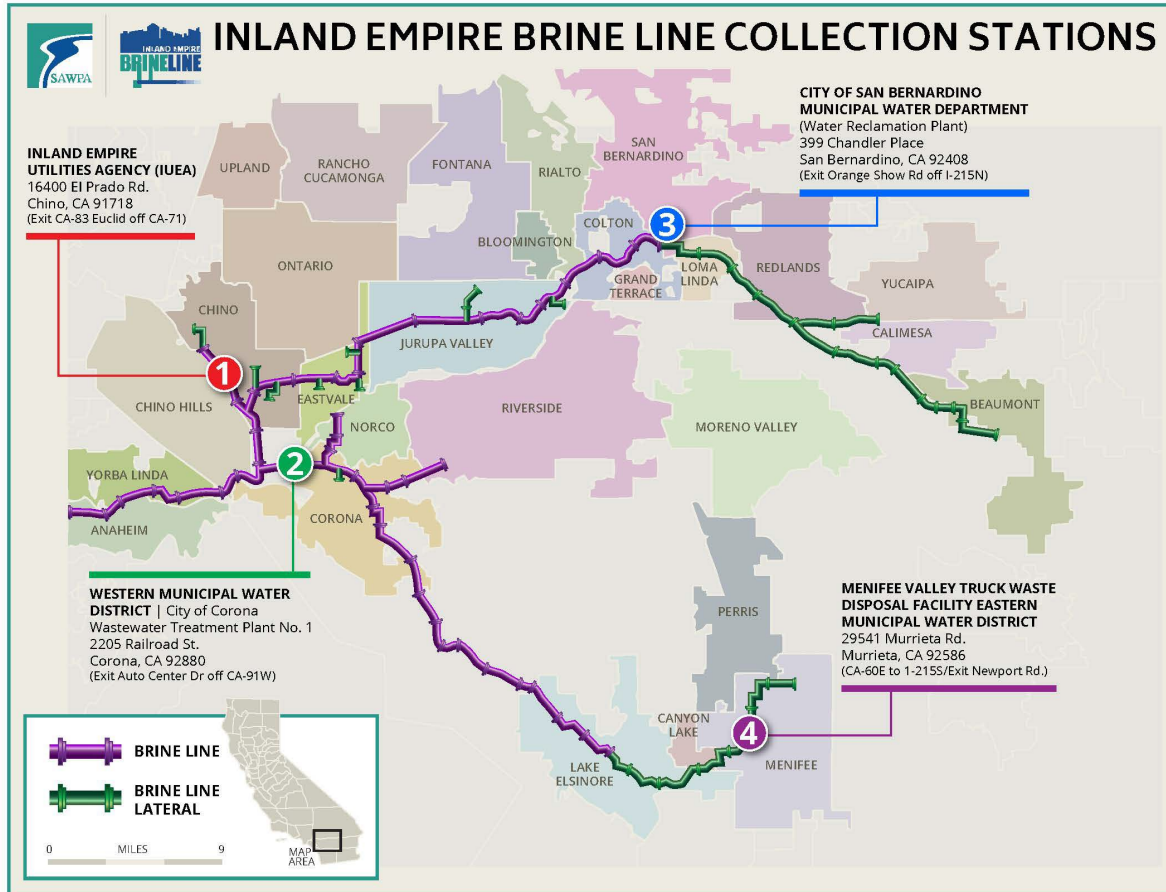
- 14 MGD
- 80% Recovery
- Feed TDS of 950 mg/L

## Goals

- Increase recovery from 80% to 90+%
- Minimize Brine Disposal Costs
  - Hard limit on brine disposal
  - Without increased recovery this also limits production
- Estimate retrofit cost and potential savings from adding 3<sup>rd</sup> RO stage

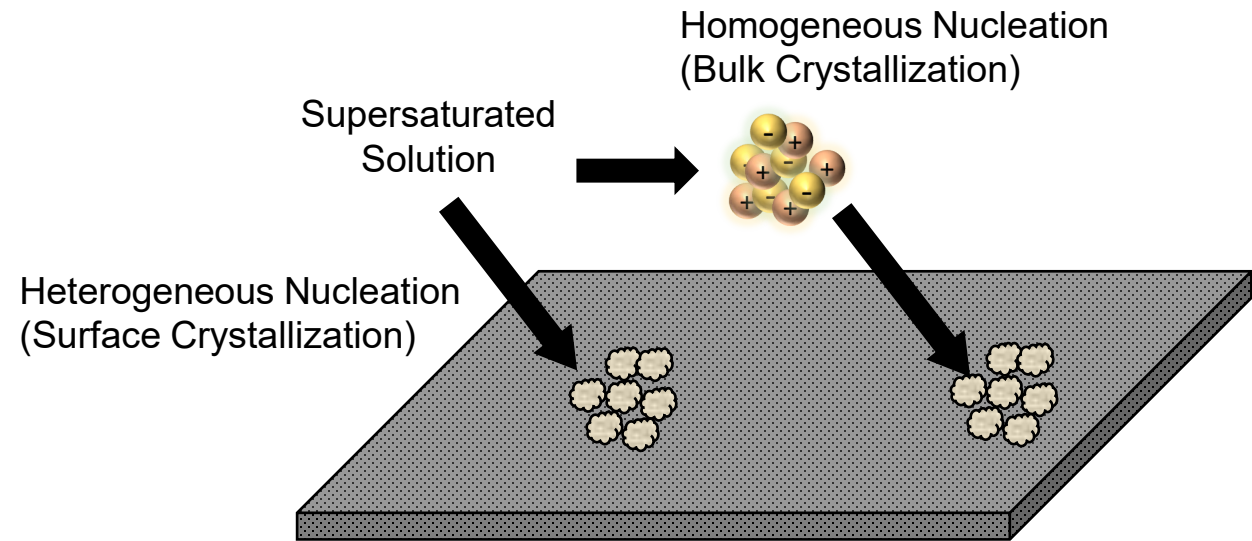
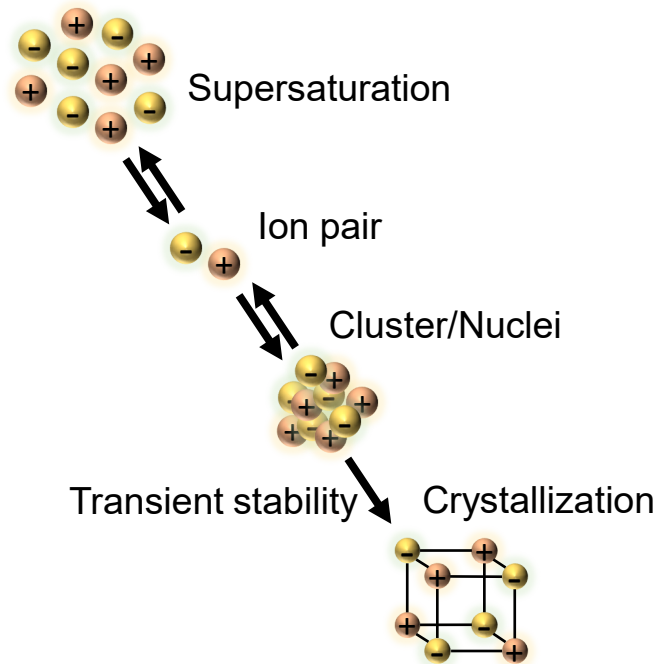


# Brine Disposal Costs and the Case For High Recovery



Fiscal Year	Flow (MG)	BOD (1,000 lbs.)	TSS (1,000 lbs.)	Monthly Fixed Pipeline	Monthly Fixed Treatment
2017	\$858	\$307	\$429	\$5,639	\$11,433
2018	\$901	\$307	\$429	\$5,921	\$12,007
2019	\$946	\$307	\$429	\$6,217	\$12,607
2020	\$979	\$316	\$442	\$6,398	\$12,985
2021 Jan - Jun	\$1,018	\$329	\$460	\$6,654	\$13,505
2021 Jul - Dec	\$979	\$316	\$442	\$6,398	\$12,985
2022 Current	\$1,018	\$329	\$460	\$6,654	\$13,505
2023 proposed	\$1,049	\$353	\$520	\$6,654	\$13,505
2024 planned	\$1,101	\$371	\$547	\$6,654	\$13,505
% Change (2017-2024)	28%	21%	28%	18%	18%

# Scaling is a multi-step and time dependent phenomena



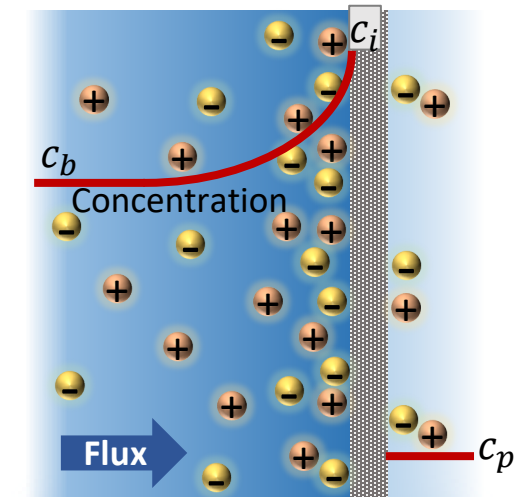
**Induction Time:** Time between the occurrences of supersaturation to the formation of stable nuclei of the precipitating salt

- Function of saturation index

$$\log t_{ind} = A + \frac{B}{T^3 SI^2}$$

## Impact of scaling

- Reduced permeability and membrane life
- Enhanced by concentration polarization



# Flow Reversal and Feed Flushing for Scaling Prevention

**Flow Reversal:** A technique to prevent scale formation by periodically reversing the flow direction in reverse osmosis (RO) systems.

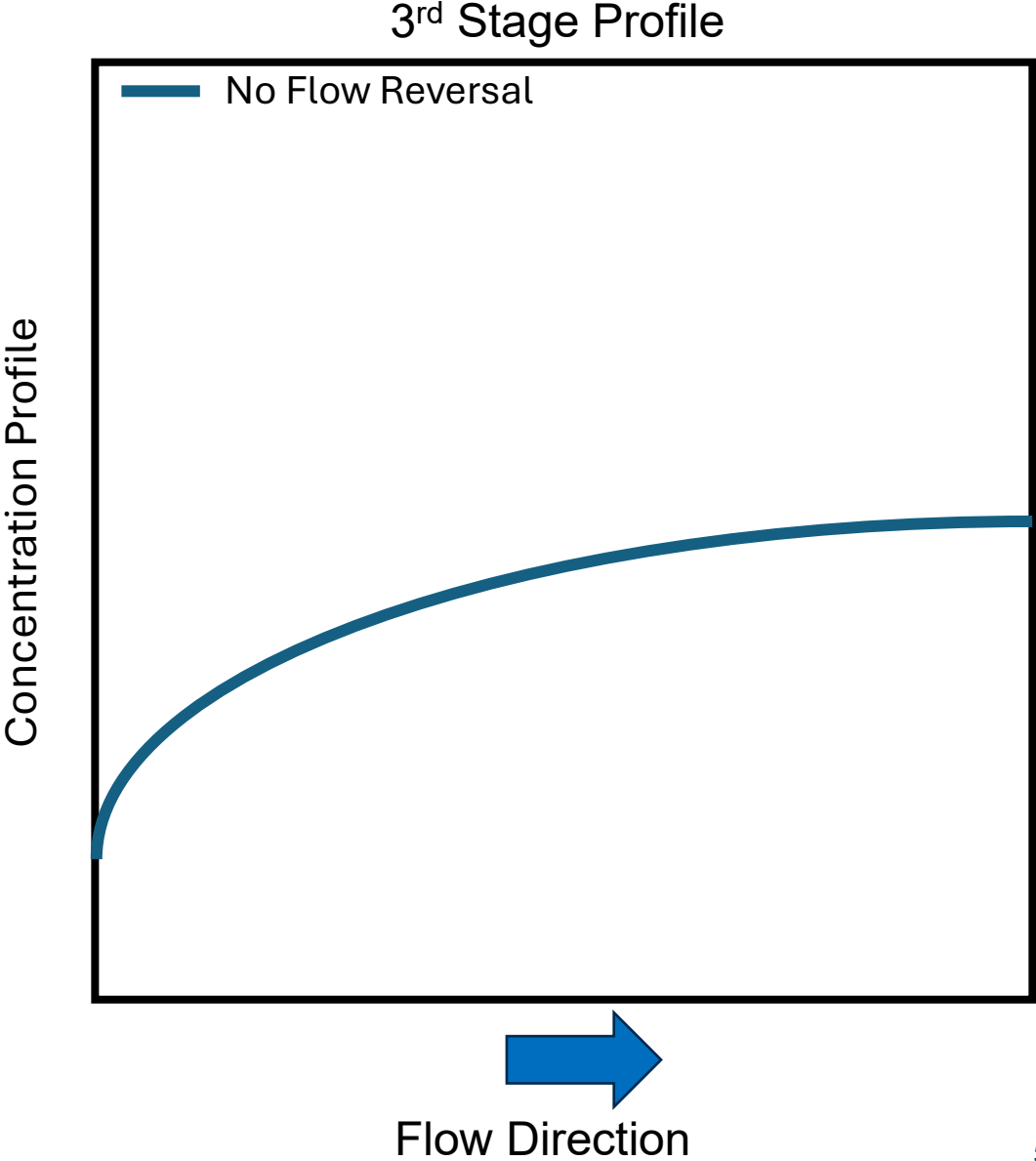
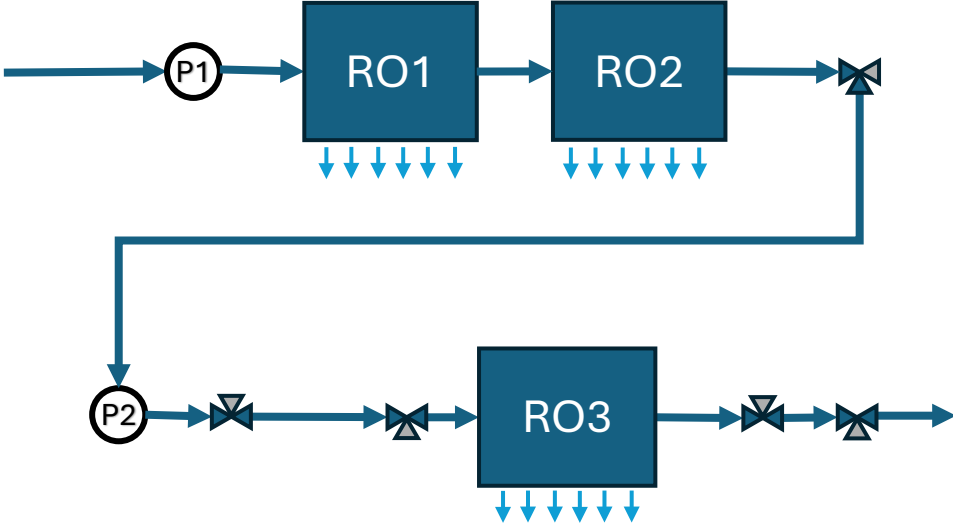
**Flushing:** Stop permeate production and flush with lower concentration water to rapidly reduce the concentration of the fluid in the system

- Resets the crystallization **induction clock**
- **Mitigates scaling**, potentially eliminating the need for antiscalants.
- **Maintains high system recovery**, even under high supersaturation conditions
- **Continuous Operation:** Unlike traditional cleaning processes, **flow reversal** minimally interrupts RO operations.

**Expected Impact:** Significantly enhances system performance, extending membrane life and improving recovery rates in RO desalination processes

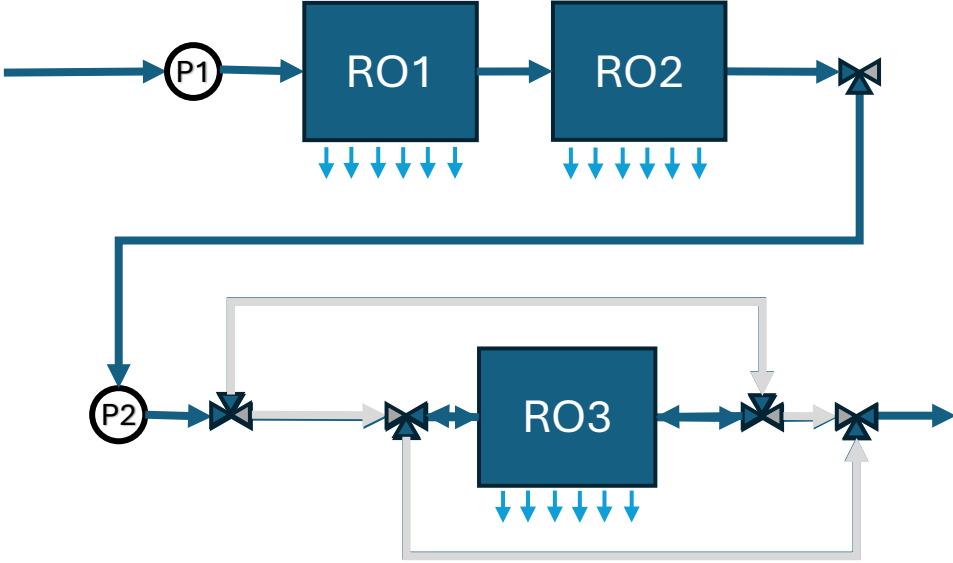
# Flow Reversal and Feed Flushing for Scale Prevention

A) Normal Operation



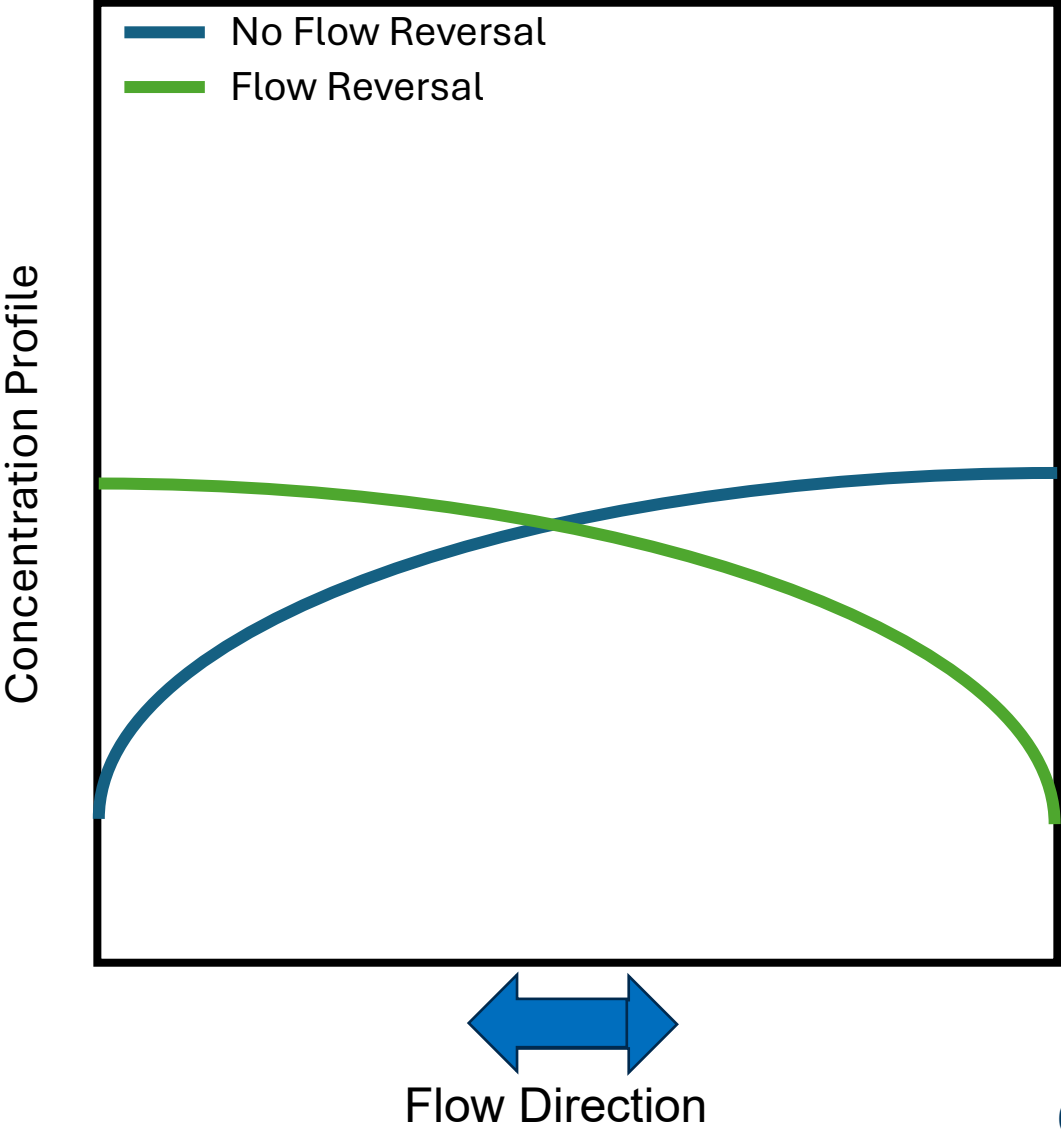
# Flow Reversal and Feed Flushing for Scale Prevention

B) Flow Reversal Operation



$$Duty Cycle = \frac{t_n}{t_n + t_s}$$

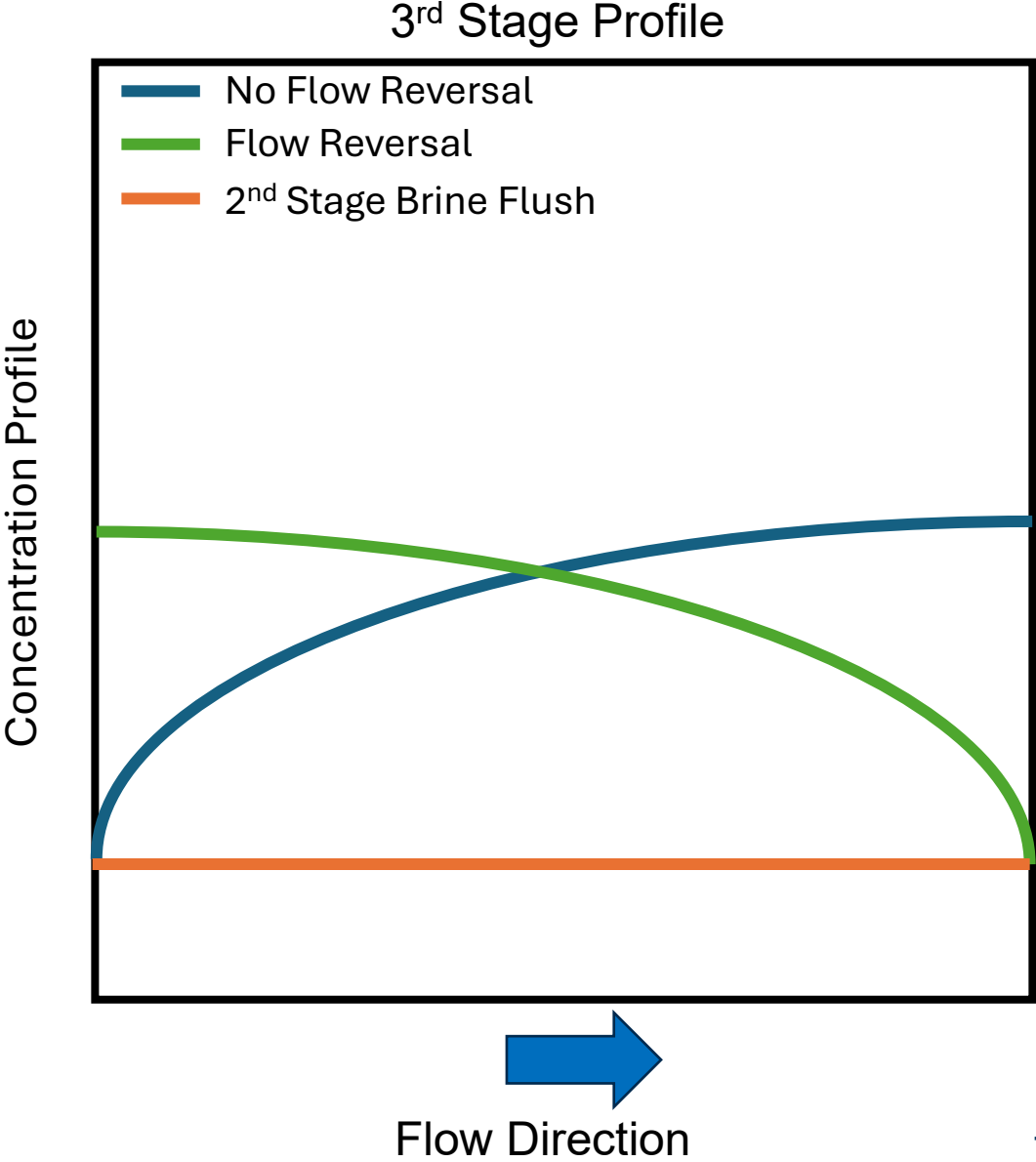
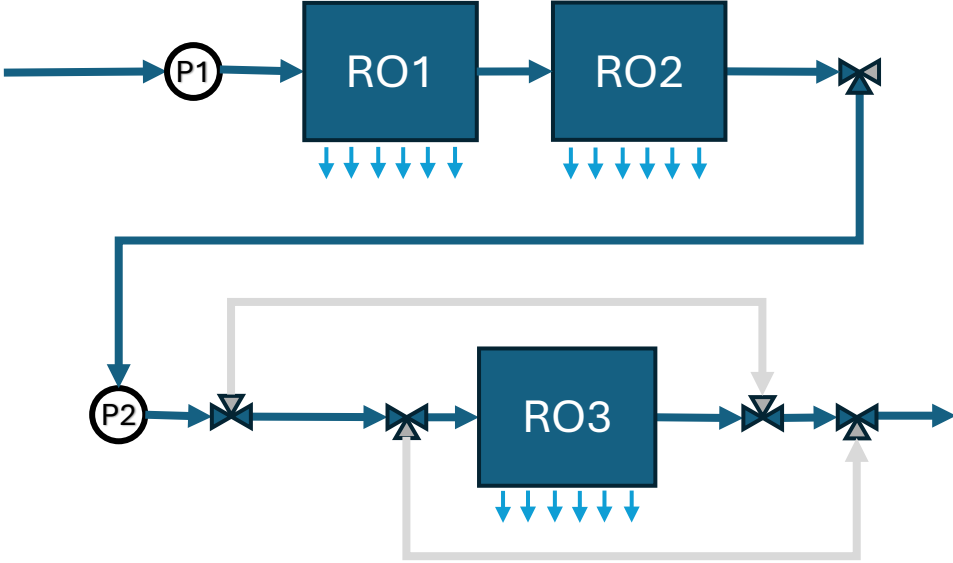
3<sup>rd</sup> Stage Profile





# Flow Reversal and Feed Flushing for Scale Prevention

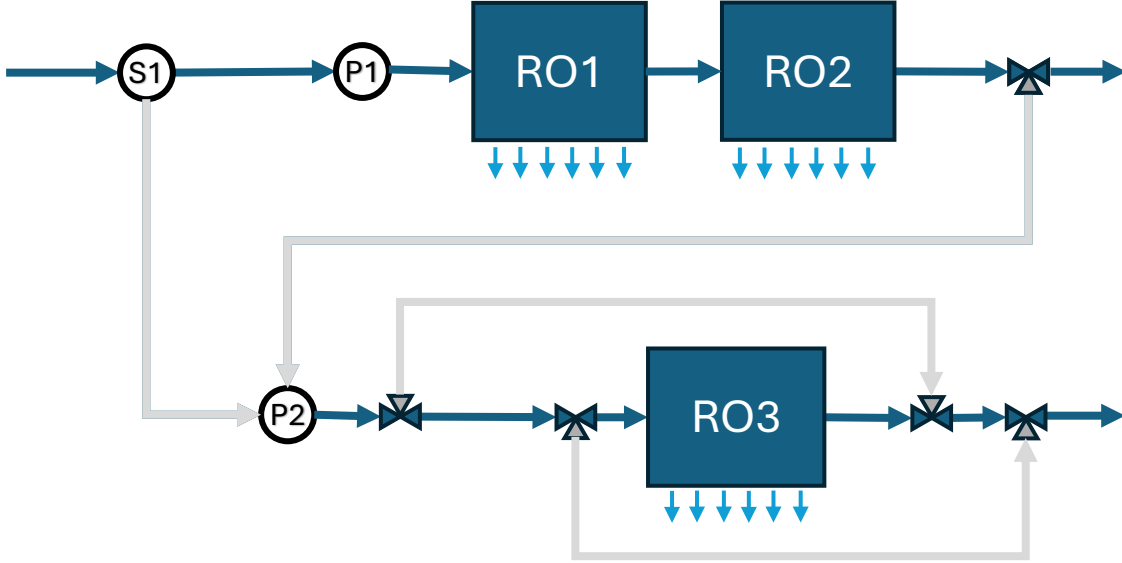
B) Brine Reversal





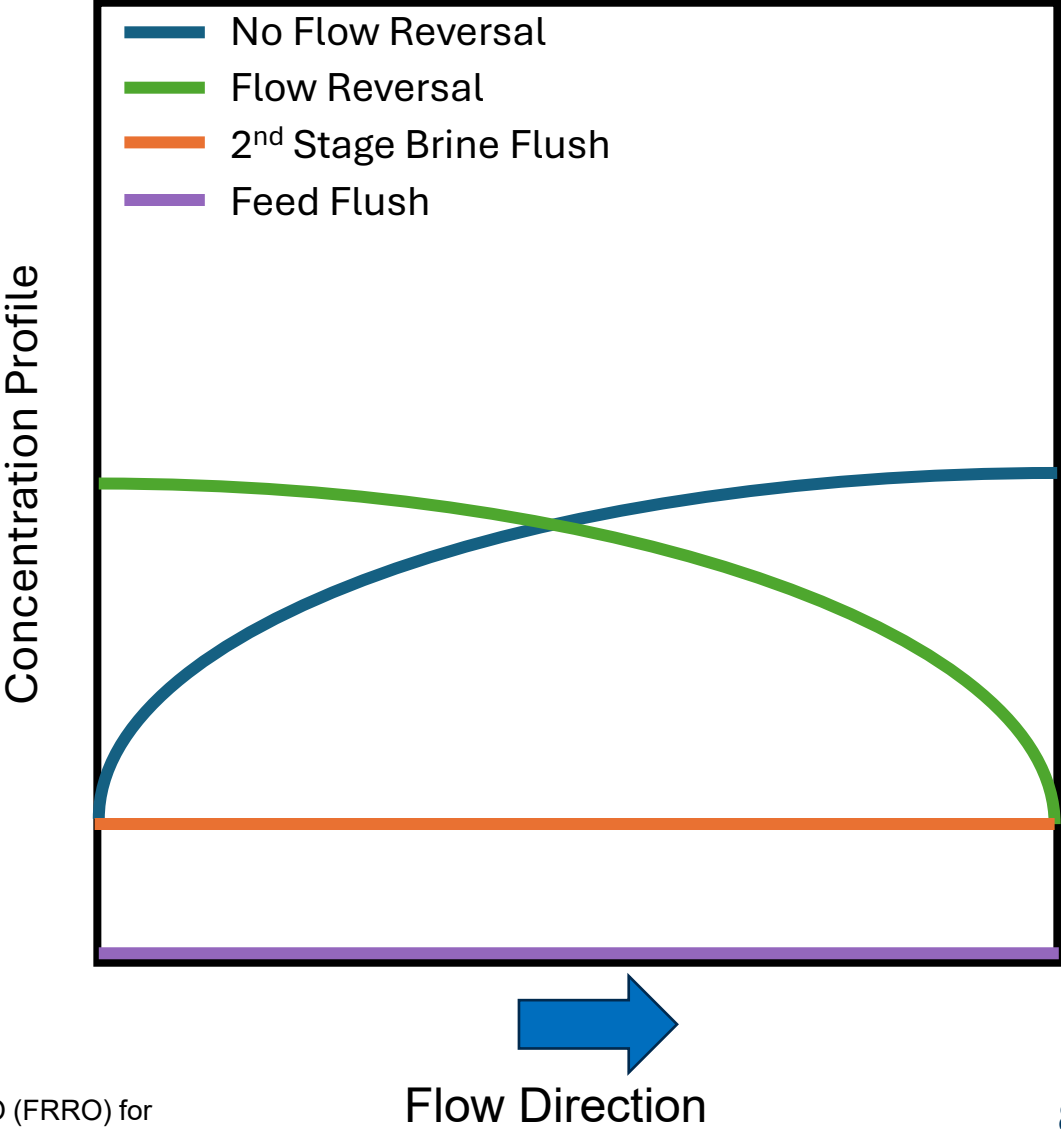
# Flow Reversal and Feed Flushing for Scale Prevention

D) Brine Flush



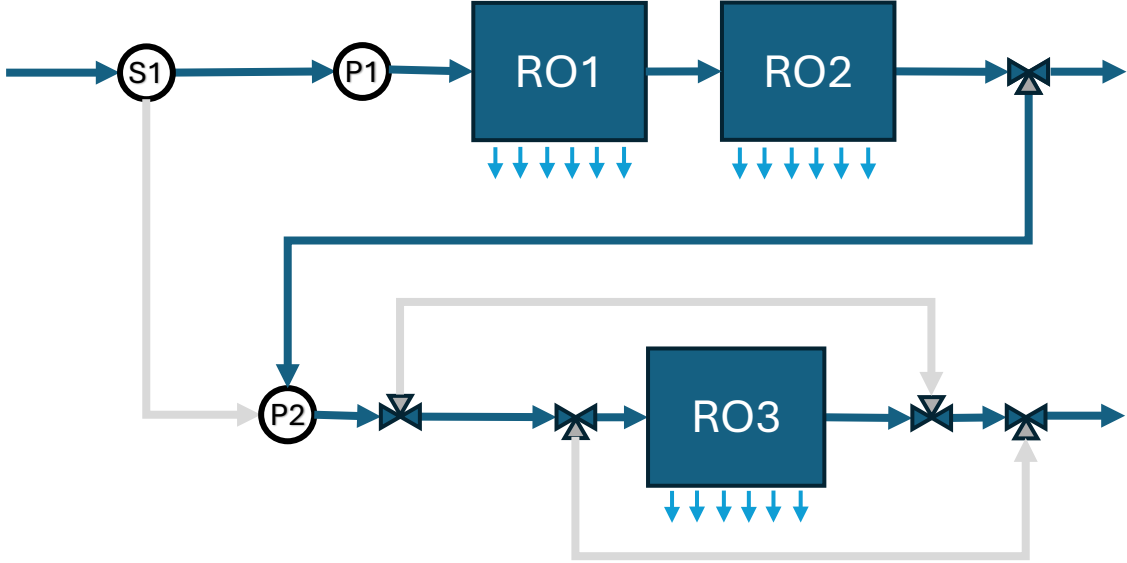
$$Flush\ Volumes = \frac{Q_{flush} t_{flush}}{V_{ch,RO3}}$$

3<sup>rd</sup> Stage Profile

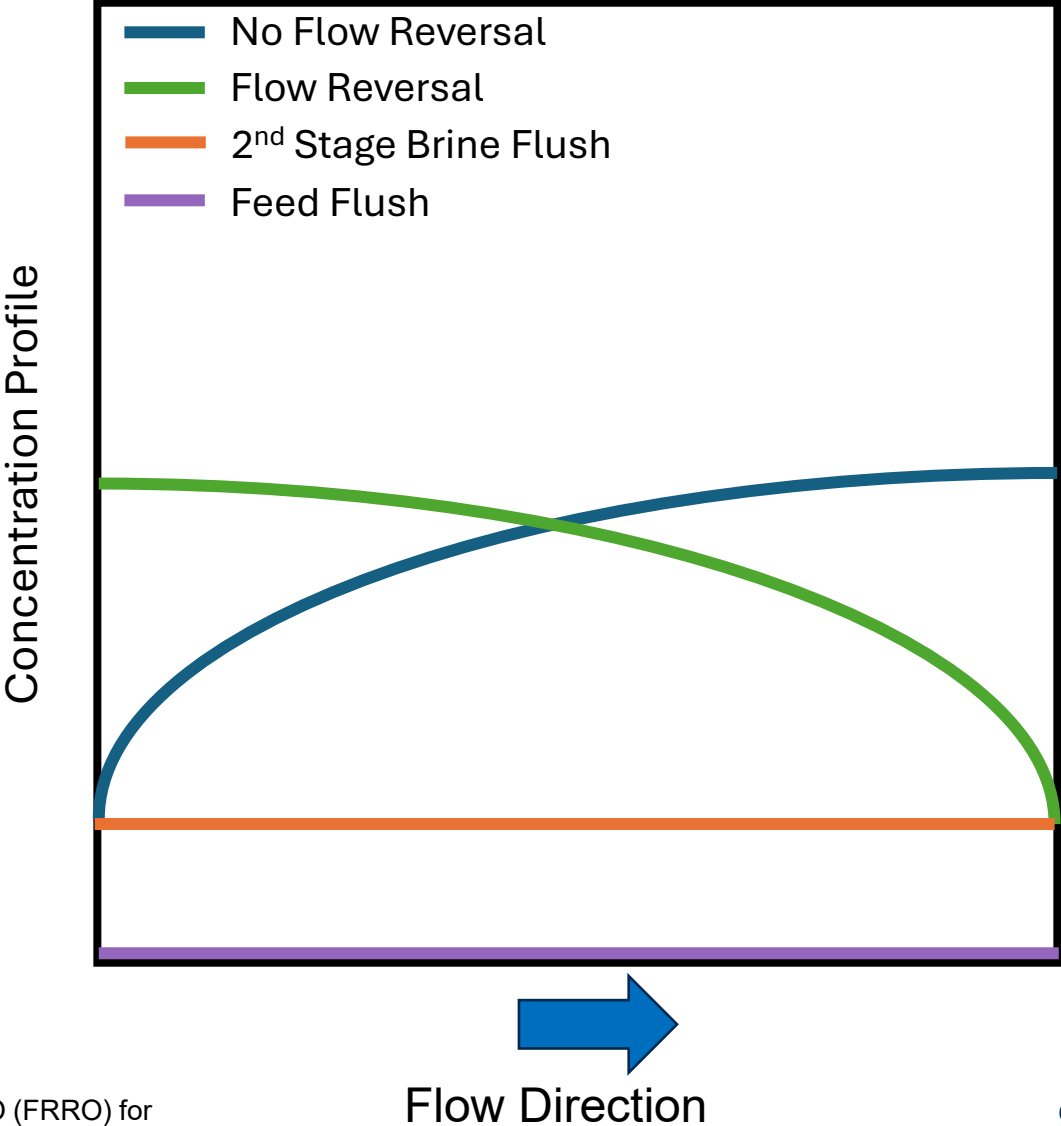


# Flow Reversal and Feed Flushing for Scale Prevention

D) Feed Flush



3<sup>rd</sup> Stage Profile



# WaterTAP Models Can Be Quickly Fit to Experimental Data Using Built-in Tools

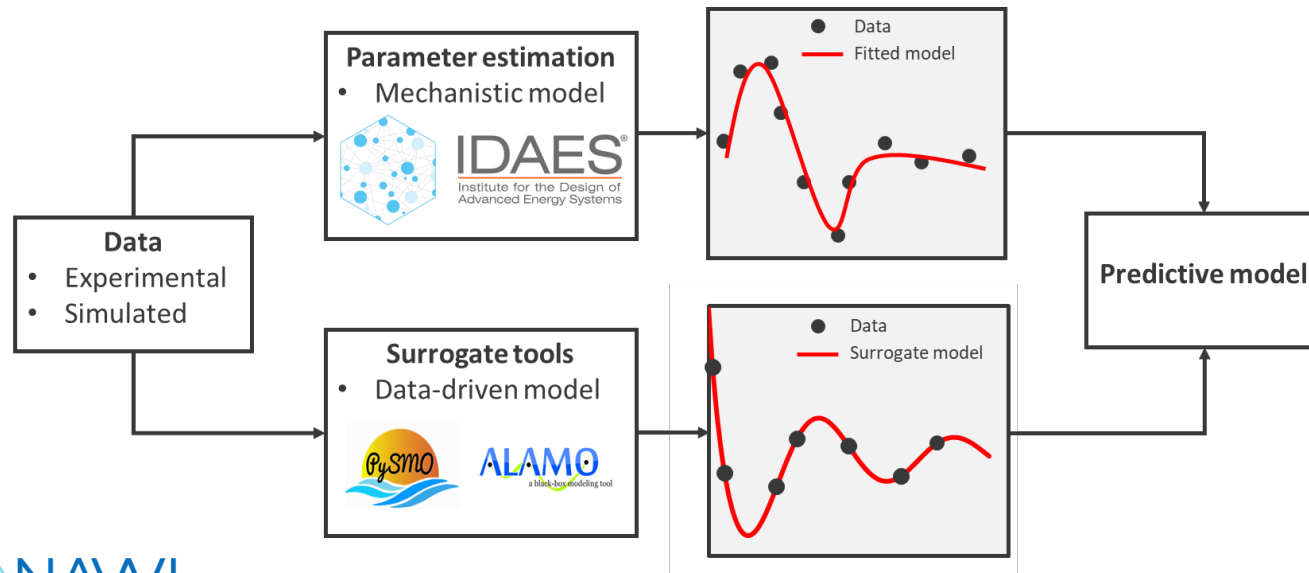
## Parmest Estimator

- WaterTAP Model
- Experiment List
- Objective Function
- Unknown Parameters
- Experimental Outputs

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## Exp. Data

Recovery (%)	$\Delta P_{RO1}$ (psi)	$\Delta P_{RO2}$ (psi)	Permeate Conc (mg/L)	Pump Work (kW)
81.1	24.6	16.7	28.7	187.4
81.0	25.6	18	28.8	190.8
.	.	.	.	.
90.5	19.4	8.1	33.5	173.6
90.5	19.5	8.2	33.7	174.3
90.4	19.6	8.1	33.8	173.6

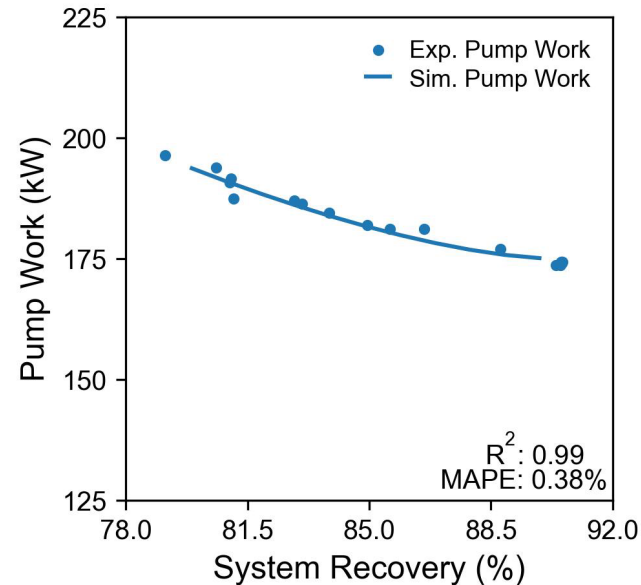
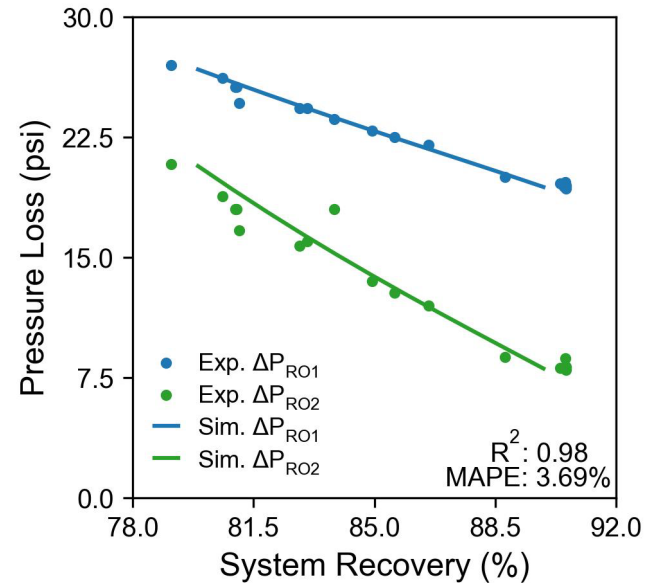
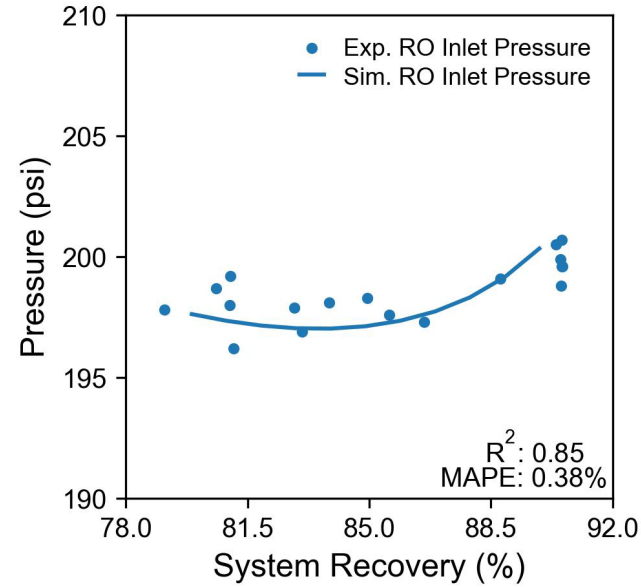
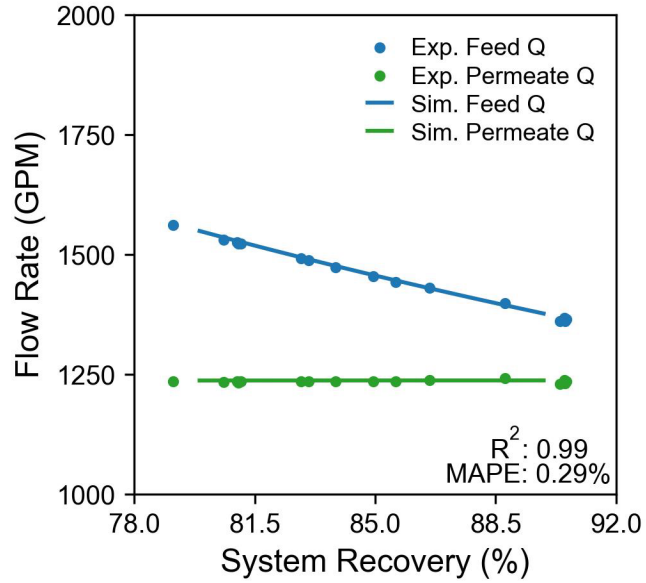


Experimental Outputs	Symbol	Units
Feed Flow Rate	$Q_f$	GPM
Permeate Flow Rate	$Q_p$	GPM
RO Feed Pressure	$P_f$	psi
RO1 Pressure Losses	$\Delta P_{RO1}$	psi
RO2 Pressure Losses	$\Delta P_{RO2}$	psi
Permeate Concentration	$C_p$	mg/L
Pump Work	$W_p$	kW



Unknown Parameters	Symbol	Units
Water permeability coefficient	$A$	$m^1 s^{-1} Pa^1$
Salt permeability coefficient	$B$	$m^1 s^{-1}$
Darcy's friction factor coefficient	$C_1$	
Darcy's friction factor exponent	$n$	
Sherwood coefficient	$C_2$	
Pump Efficiency	$\xi$	%

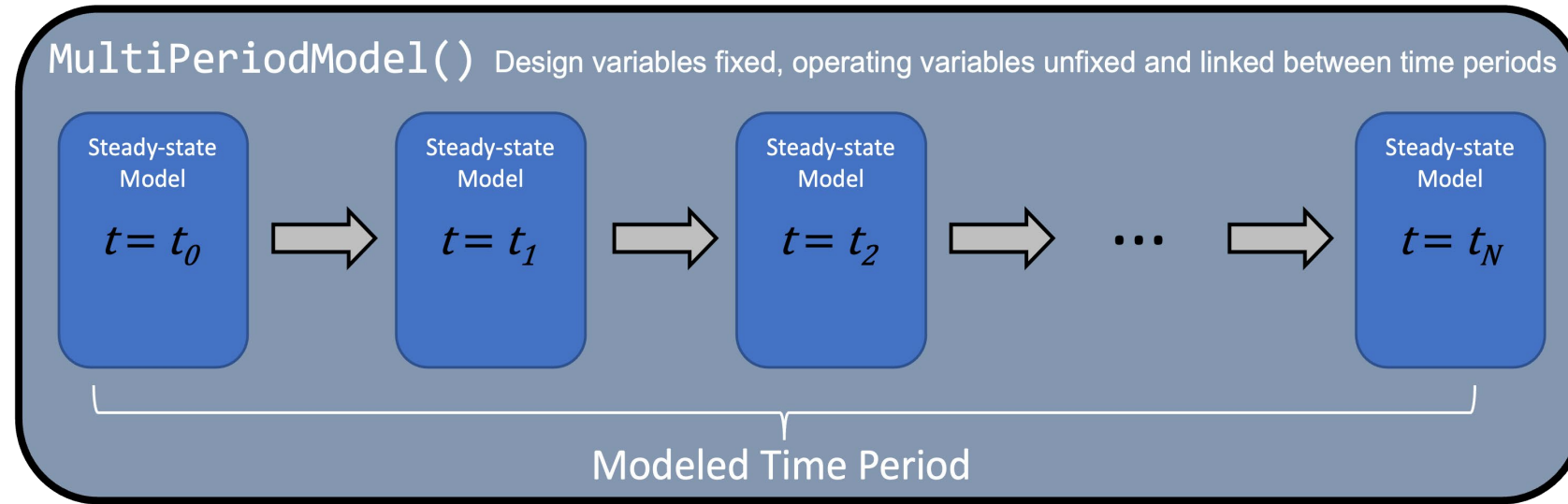
# Experimental Data and Parameter Estimation Results



Parameter	Symbol	Value	Units
Water permeability coefficient	$A$	8.80e-12	$\text{m}^1 \text{s}^{-1} \text{Pa}^1$
Salt permeability coefficient	$B$	8.00e-08	$\text{m}^1 \text{s}^{-1}$
Darcy's friction factor coefficient	$C_1$	7.82	dimensionless
Darcy's friction factor exponent	$n$	0.354	dimensionless
Sherwood coefficient	$C_2$	4.73	dimensionless
Pump Efficiency	$\xi$	65.1	%

Metric	$R^2$	MAPE (%)
Flow Rates ( $Q_f + Q_p$ )	0.99	0.29
Pump Pressure ( $P_f$ )	0.85	0.38
Pressure Losses ( $\Delta P_{R01} + \Delta P_{R02}$ )	0.98	3.89
Permeate Concentration ( $C_p$ )	0.91	8.11
Pump Work ( $W_p$ )	0.99	0.38

# Multiperiod Model Unlocks Optimization Across Operating Modes



## Multiperiod Constraints:

- System Recovery
- Product Quality
- Flush Time/Duty
- Membrane Lifetime

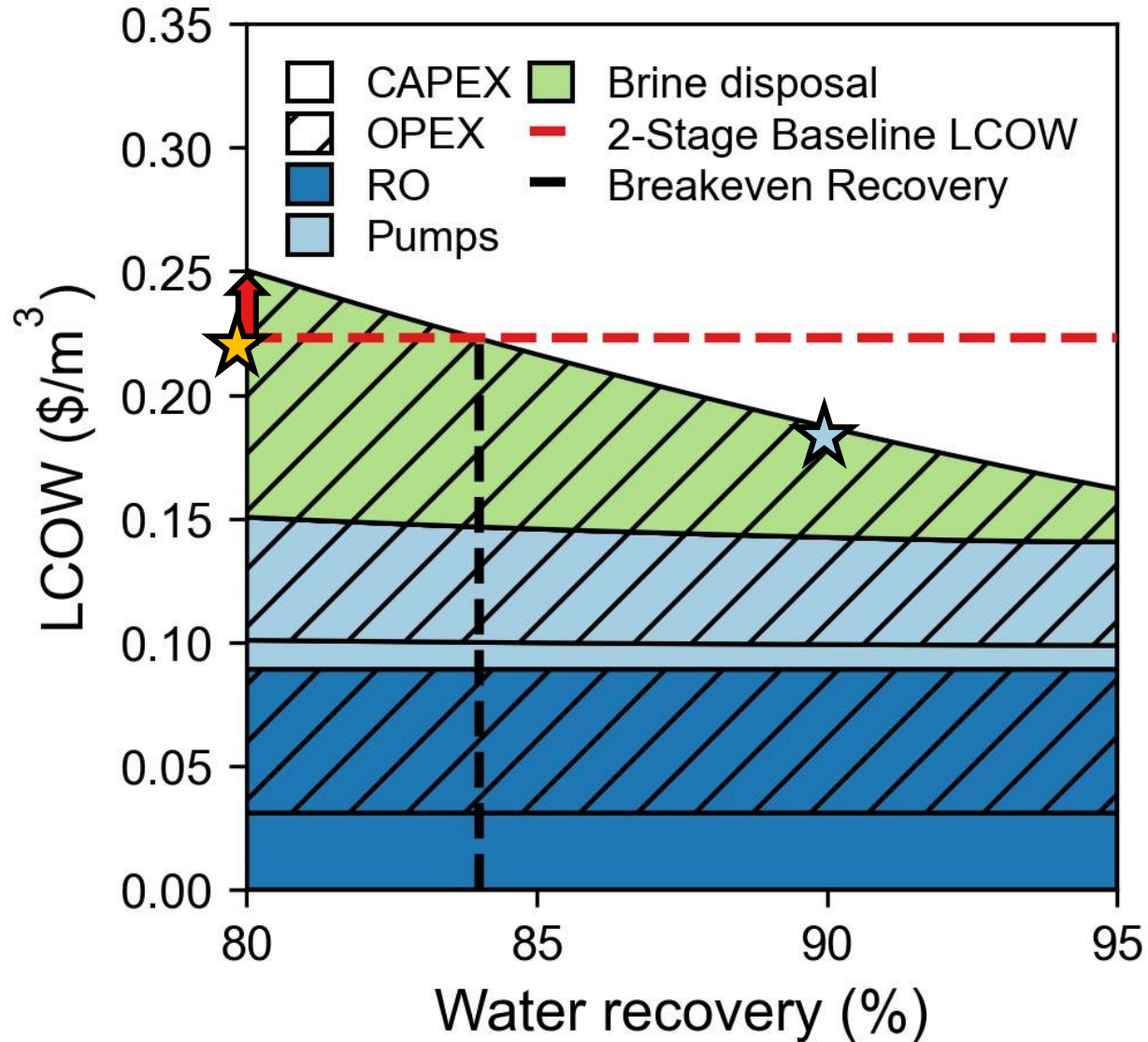
## Multiperiod Objectives:

$$\min \sum_{x \in X} [LCOW(x) * D(x)]$$

## Results:

- Results for  $t_0 - t_n$
- Net Results

# Retrofit Increases Capital Cost But Unlocks Higher Recovery

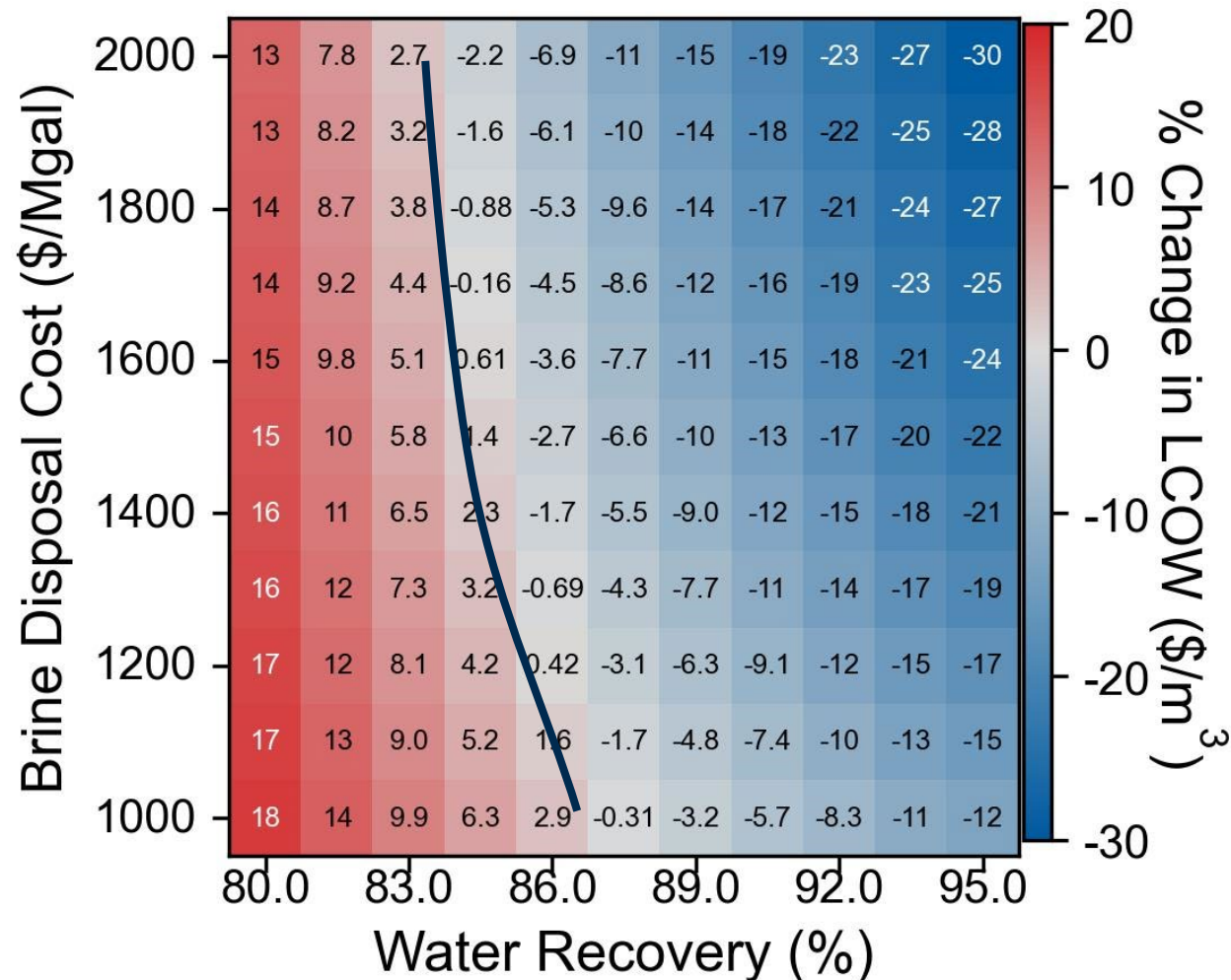


	2-Stage Baseline (80%)	3-Stage FFRRO (90%)
Total Capital Cost	\$909,604	\$1,061,951
Total Operating Cost	\$457,492	\$359,695
- Brine Disposal Cost	\$245,787	\$109,876
Total Annualized Cost	\$548,452	\$460,874
LCOW	\$0.223	\$0.187

Assumptions:	
Flow Reversal Duty Cycle	95%
3 <sup>rd</sup> Stage Membrane Life	1 Yr.
Brine Disposal Cost	\$1500/MGallon



# Disposal Costs Are A Primary Driver for Operation



**Key Takeaway:** As disposal costs increase it is critical to increase recovery.

- As disposal costs increase, the capital cost investment becomes less of a burden.

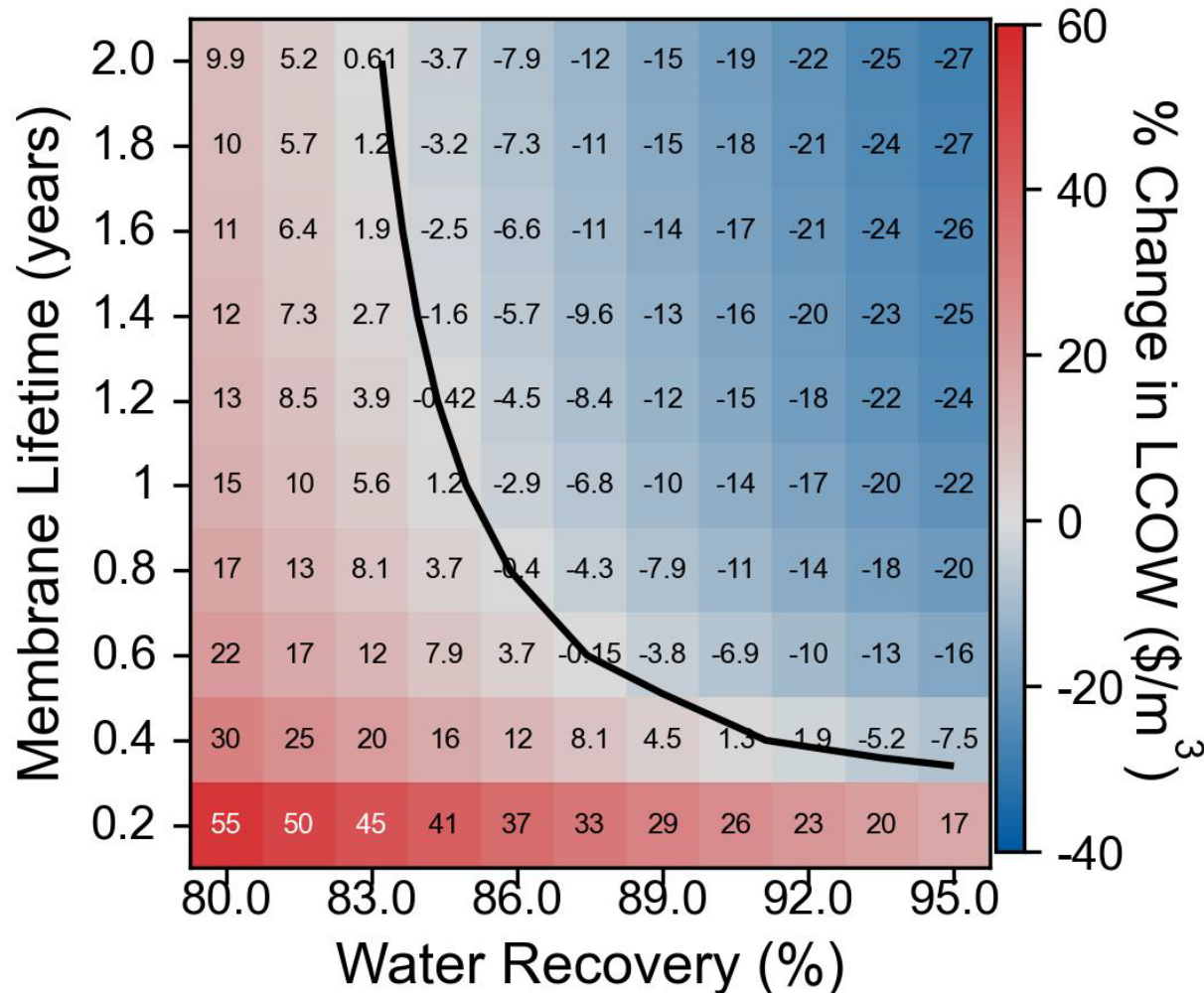
Assumptions: Flow Reversal

Flow Reversal Duty Cycle 95%

3<sup>rd</sup> Stage Membrane Life 1 Yr.



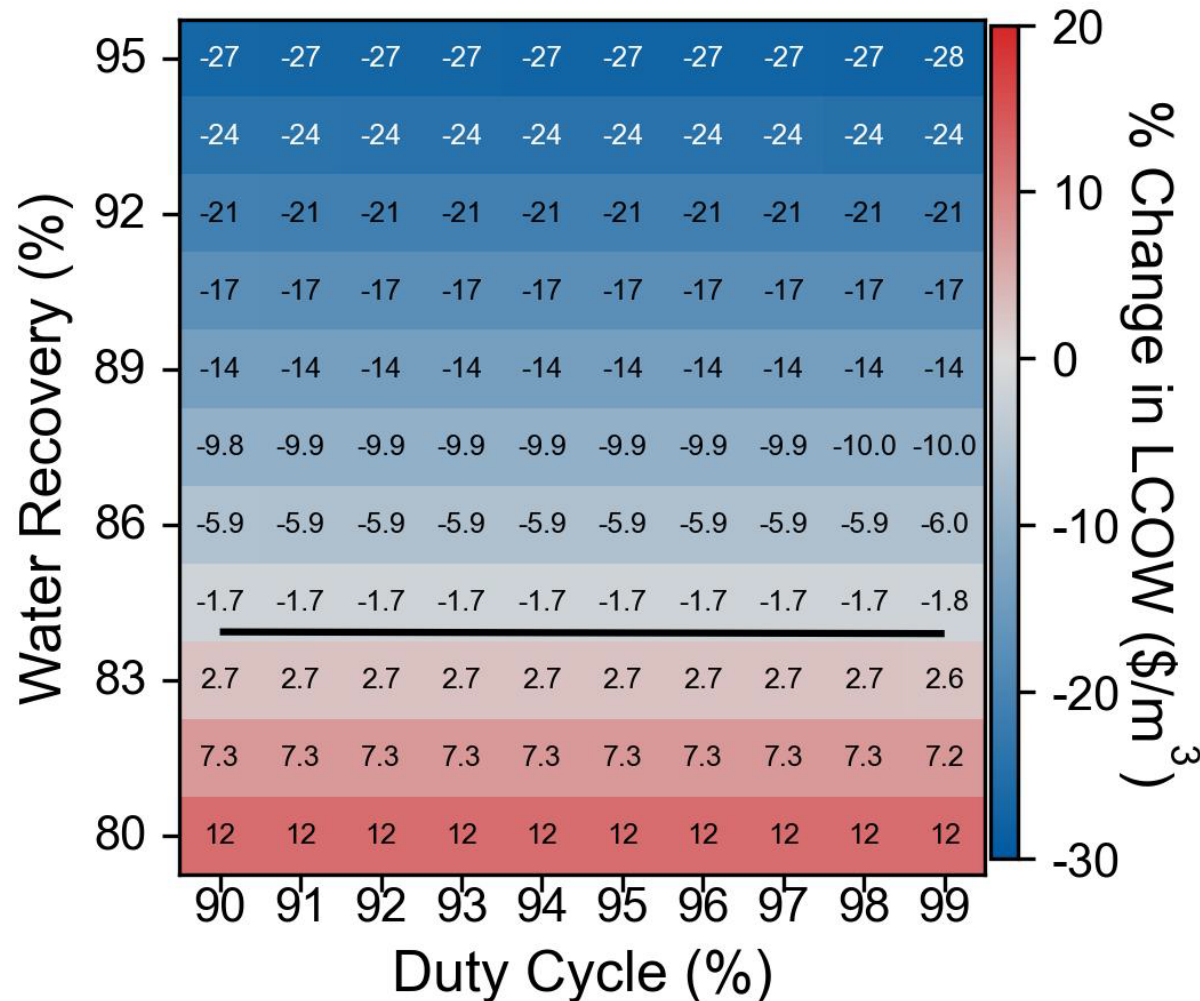
# Increasing Recovery Offsets Retrofit Cost If Membrane Lifetime Improves



**Key Takeaway:** Flow reversal or feed flushing can see positive returns if they can increase membrane lifetime at higher recoveries.

Assumptions: Flow Reversal  
 Flow Reversal Duty Cycle 95%  
 Brine Disposal Cost \$1500/MGallon

# Duty Cycle Has Minimal Impact on LCOW



**Key Takeaway:** The duty cycle for flow reversal doesn't impact system costs very much.

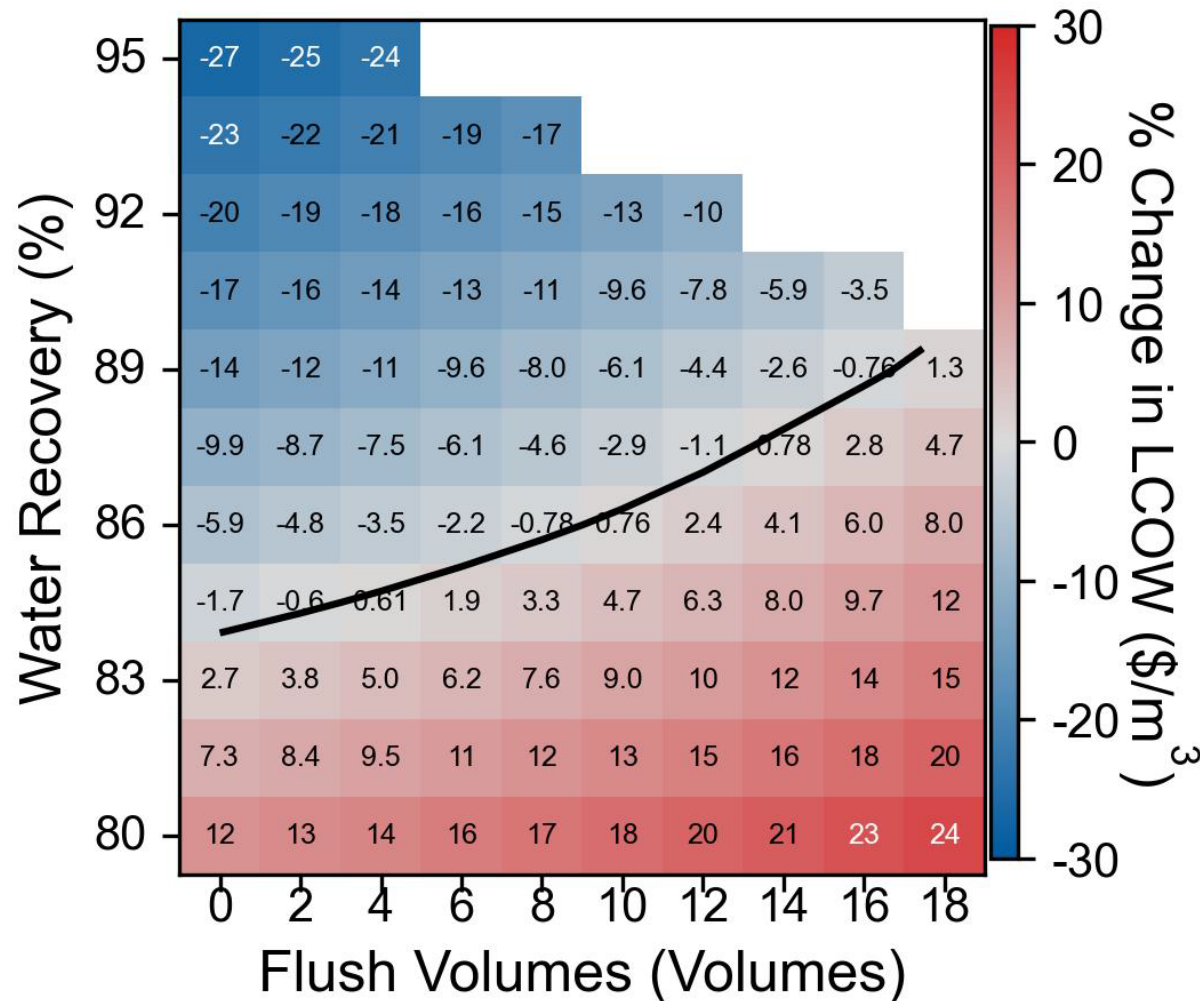
- Stage 3 recovers the last ~10% and is down  $\leq 10\%$  of the time. These losses can easily be made-up during the rest of the duty cycle.

Assumptions: Flow Reversal

Brine Disposal Cost           \$1500/MGallon

3<sup>rd</sup> Stage Membrane Life    1 Yr.

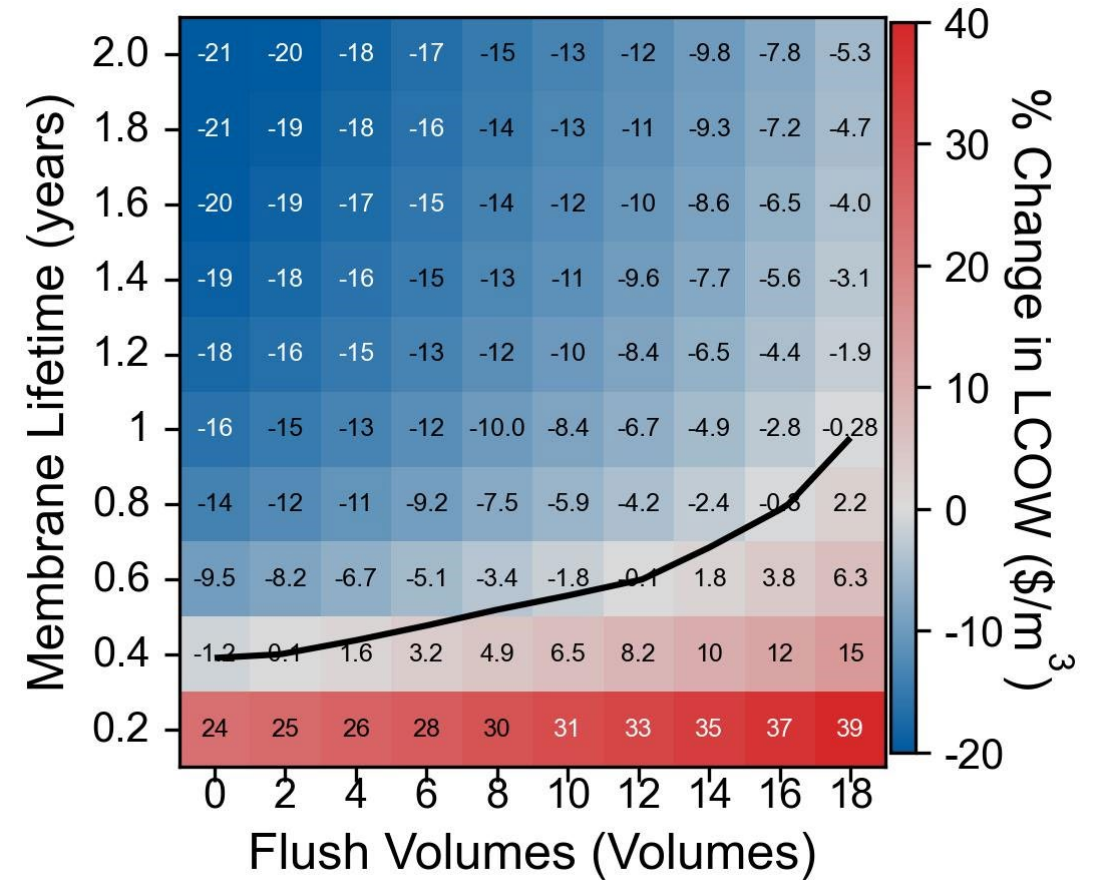
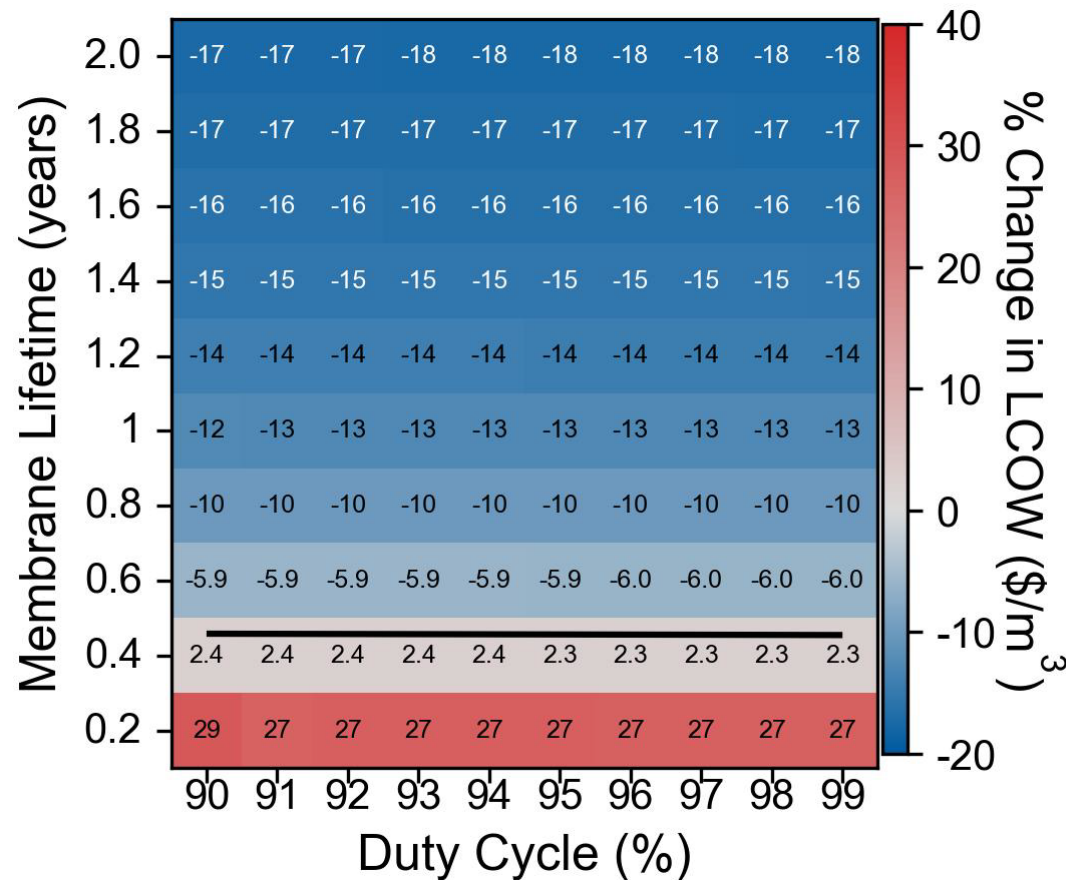
# The Impact of Flow Reversal and Flushing is Minimal Compared to Recovery



**Key Takeaway:** The wasted flush volumes are expensive compared to flow reversal, but can be offset by increased recovery and may be more effective in resetting induction time.

Assumptions: Feed Flushing  
 Brine Disposal Cost \$1500/MGallon  
 3<sup>rd</sup> Stage Membrane Life 1 Yr.

# The Relationship Between Flow Reversal, Flushing, and Membrane Life Is Critical



## Assumptions:

Water Recovery 90%

Brine Disposal Cost \$1500/MGallon



# Conclusions

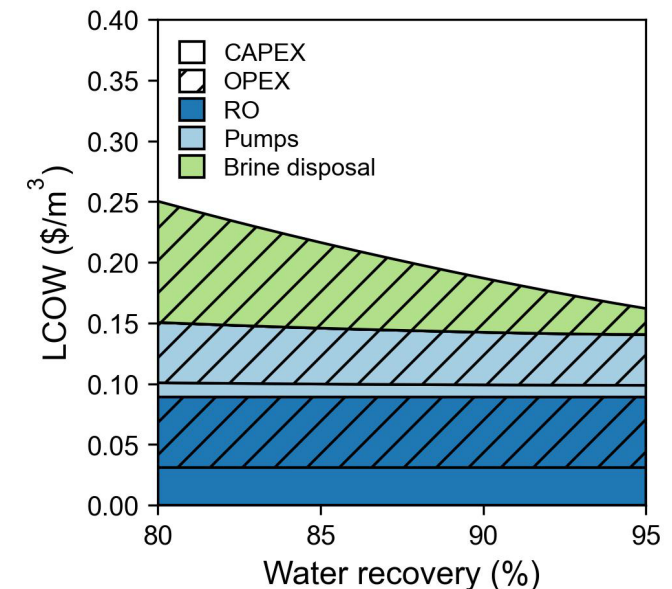
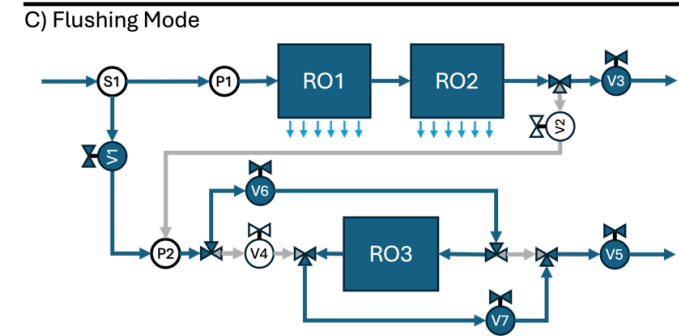
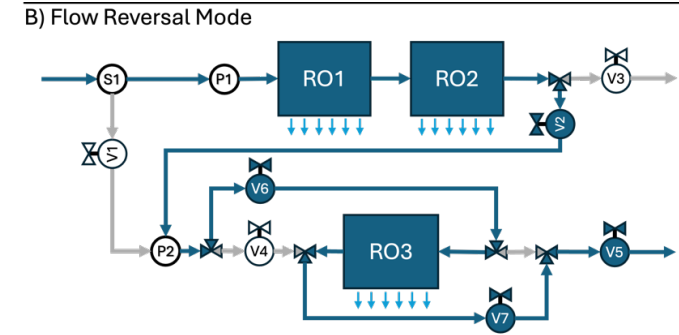
**High Recovery:** Implementing a 3rd RO stage process can increase recovery rates at Chino I beyond 90%, significantly reducing brine disposal costs.

**Economic Viability:** Retrofit costs are offset by reduced brine disposal costs.

**Key Factor:** The impact of flow reversal and flushing frequency on membrane life is critical in ensuring long-term process sustainability and estimating system performance.

**Future Work:** Reaktor will be integrated to model the impact of flow reversal and feed flushing on membrane lifetime.

- Move beyond sensitivity analysis and perform system optimization



# Thank You

